

Set-Membership identification of linear systems with input backlash

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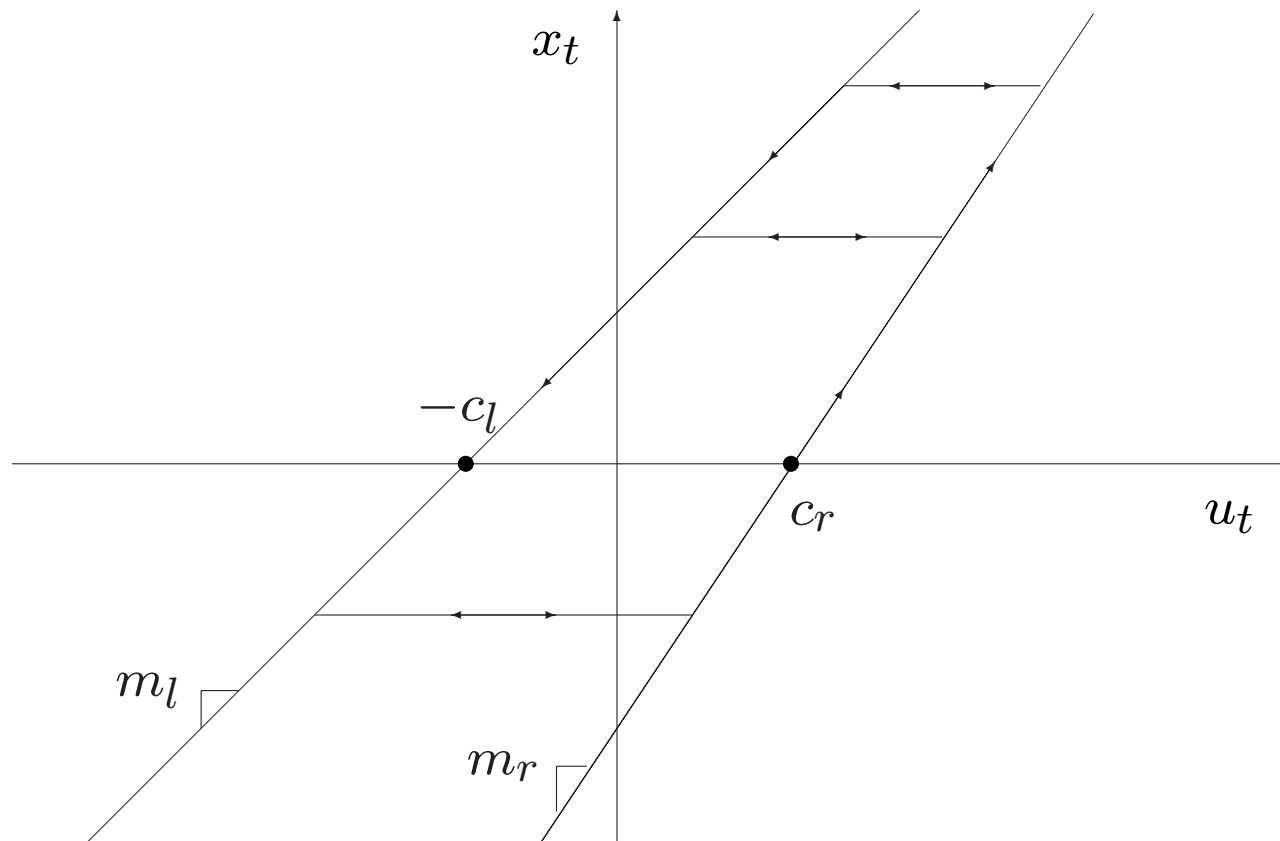
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*Scuola di Dottorato SIDRA "A. Ruberti" 2007
Identificazione di sistemi nonlineari
Bertinoro, 9-11 Luglio 2007*

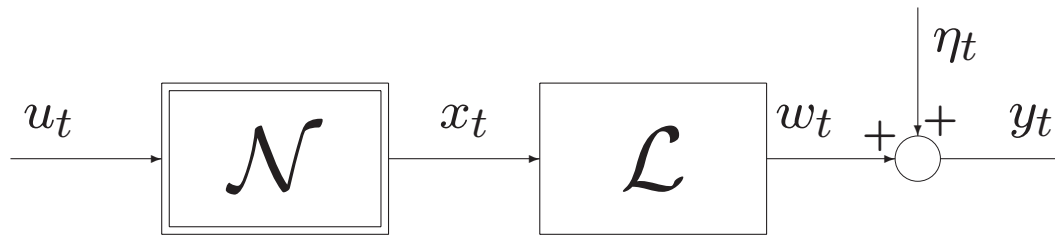
Backlash nonlinearity

- Backlash is a **hard** (i.e. non-differentiable) and **dynamic** (i.e. with memory) nonlinearity.
- Backlash is a **typical characteristic of mechanical connections** (e.g. gearboxes).



Linear systems with input backlash

- The structure resemble that of **Hammerstein systems**
- **Backlash** nonlinearity is considered **instead of** the usual **memoryless nonlinearity**



where:

\mathcal{N} : backlash nonlinearity

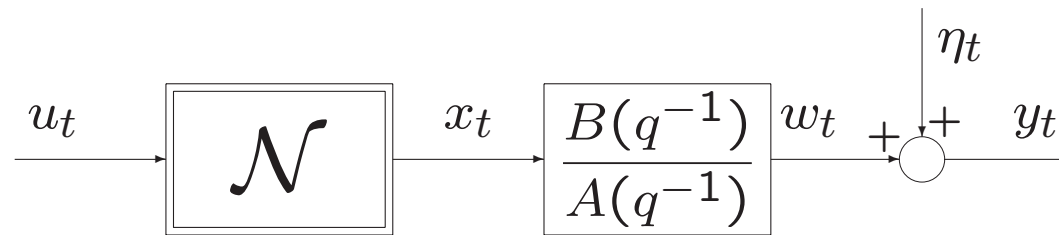
\mathcal{L} : linear subsystem

x_t : inner signal **not measurable**

Identification of linear systems with input backlash

- Motivations:
 - **Backlash** severely **limits** the **performance** of control systems (may cause delays, oscillations, limit cycles, inaccuracy, ...)
 - **Adaptive** and/or **robust control** techniques **can cope** with such limitations.
 - **Robust control** techniques **need bounds** on the parameters of uncertain backlash (see, e.g., M. Corradini et al., “A VSC approach for the robust stabilization of nonlinear plants with uncertain non-smooth actuator nonlinearities — A unified framework”, IEEE TAC 2004)
 - Identification approach:
 - Statistical framework:
E.W. Bai, “Identification of linear system with hard input nonlinearity”, *Automatica* 2002
 - Set-membership framework: focus of this lesson
-

Problem formulation



$$x_t = \begin{cases} m_l(u_t + c_l) & \text{for } u_t \leq z_l \\ m_r(u_t - c_r) & \text{for } u_t \geq z_r \\ x_{t-1} & \text{for } z_l < u_t < z_r \end{cases}$$

$$m_l > 0, m_r > 0, c_l > 0, c_r > 0$$

$$z_l = \frac{x_{t-1}}{m_l} - c_l, \quad z_r = \frac{x_{t-1}}{m_r} + c_r$$

$$A(q^{-1}) = 1 + a_1q^{-1} + \dots + a_{na}q^{-na}$$

$$B(q^{-1}) = b_0 + b_1q^{-1} + \dots + b_{nb}q^{-nb}$$

$$q^{-1}w_t = w_{t-1}$$

Problem formulation

- **Aim:** compute **bounds** on the parameters $\gamma^T = [m_l \ c_l \ m_r \ c_r]$ and $\theta^T = [a_1 \ \dots \ a_{na} \ b_0 \ \dots \ b_{nb}]$.
- **Prior assumption on the system:**
 1. **stability**;
 2. na and nb are **known**;
 3. the **steady-state gain** is **not zero**;
 4. a rough **upper bound** on the **settling time** of the system is known;
- **Prior assumption on the measurement uncertainty:**
 1. $\{\eta_t\}$ is UBB: $\|\{\eta_t\}\|_\infty \leq \Delta\eta_t$;
 2. $\Delta\eta_t$ is **known**;

Proposed solution: preliminary

Three-stage solution:

- **First stage:** computation of **bounds** on the **backlash** parameters γ .
- **Second stage:** computation of **bounds** on the **inner (unmeasurable) signal** x_t .
- **Third stage:** computation of **bounds** on the **linear block** parameters θ .

Proposed solution: preliminary

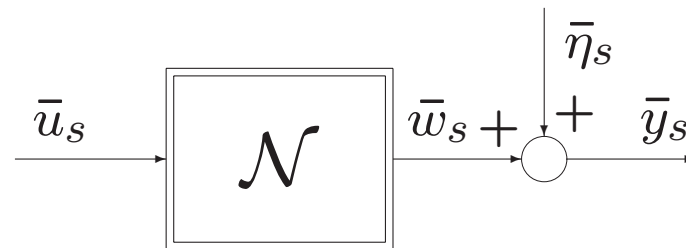
Remark 1: The parameterization is not unique

$$\Rightarrow \text{assume } g_{dc} = \frac{\sum_{j=0}^{nb} b_j}{1 + \sum_{i=1}^{na} a_i} = 1$$

Remark 2: Stimulate the system with a set of **square wave inputs** with **different amplitudes**



Steady-state operating conditions:



Proposed solution: first-stage

1) Bounds on the backlash parameters

- Get $M \geq 2$ steady-state measurements:

$$\bar{y}_i = m_r(\bar{u}_i - c_r) + \bar{\eta}_i, \quad \text{for } \bar{u}_i \geq \frac{\bar{x}_{i-1}}{m_r} + c_r \quad i = 1, \dots, M$$

$$\bar{y}_j = m_l(\bar{u}_j + c_l) + \bar{\eta}_j, \quad \text{for } \bar{u}_j \leq \frac{\bar{x}_{j-1}}{m_l} - c_l \quad j = 1, \dots, M$$

- The *feasible parameter set* of the backlash, is defined by the following equations:

$$\mathcal{D}_\gamma = \mathcal{D}_\gamma^r \cup \mathcal{D}_\gamma^l$$

$$\mathcal{D}_\gamma^r = \{m_r, c_r \in R^+ : \bar{y}_i = m_r(\bar{u}_i - c_r) + \bar{\eta}_i, |\bar{\eta}_i| \leq \Delta \bar{\eta}_i; \quad i = 1, \dots, M\} \quad (1)$$

$$\mathcal{D}_\gamma^l = \{m_l, c_l \in R^+ : \bar{y}_j = m_l(\bar{u}_j + c_l) + \bar{\eta}_j, |\bar{\eta}_j| \leq \Delta \bar{\eta}_j; \quad j = 1, \dots, M\} \quad (2)$$

Proposed solution: preliminary

Remarks:

- $\mathcal{D}_\gamma = \mathcal{D}_\gamma^r \cup \mathcal{D}_\gamma^l$ exactly described by the following nonlinear constraints

$$\bar{y}_i - m_r(\bar{u}_i - c_r) \geq -\Delta\bar{\eta}_i, \quad \bar{y}_i - m_r(\bar{u}_i - c_r) \leq \Delta\bar{\eta}_i, \quad m_r > 0, c_r > 0, i = 1, \dots, M$$

$$\bar{y}_j - m_l(\bar{u}_j + c_l) \geq -\Delta\bar{\eta}_j, \quad \bar{y}_j - m_l(\bar{u}_j + c_l) \leq \Delta\bar{\eta}_j, \quad m_l > 0, c_l > 0, j = 1, \dots, M$$
- \mathcal{D}_γ^l and \mathcal{D}_γ^r are disjoint sets (they can be handled separately).
- \mathcal{D}_γ^l and \mathcal{D}_γ^r have the same mathematical structure (enjoy the same properties).
- Results derived for \mathcal{D}_γ^r in the following slides, are also applicable to \mathcal{D}_γ^l .

Proposed solution: first-stage

Definition 1 (Constraints boundaries defining \mathcal{D}_γ^r)

the **constraints defining** the \mathcal{D}_γ corresponding to the s -th sets of data (\bar{u}_s, \bar{y}_s) are:

$$\begin{aligned} h_r^+(\bar{u}_s) &\doteq \{m_r \in R^+, c_r \in R^+ : \bar{y}_s + \Delta\eta_s = m_r(\bar{u}_s - c_r)\} \\ h_r^-(\bar{u}_s) &\doteq \{m_r \in R^+, c_r \in R^+ : \bar{y}_s - \Delta\eta_s = m_r(\bar{u}_s - c_r)\} \end{aligned}$$

Definition 2 (Boundary of \mathcal{D}_γ^r)

$$\text{Boundary of } \mathcal{D}_\gamma^r \doteq \mathcal{H}(\mathcal{D}_\gamma^r)$$

Definition 3 (Edges of \mathcal{D}_γ^r)

$$\tilde{h}_r^+(\bar{u}_s) \doteq h_r^+(\bar{u}_s) \cap \mathcal{D}_\gamma^r = \{m_r, c_r \in \mathcal{D}_\gamma^r : \bar{y}_s + \Delta\eta_s = m_r(\bar{u}_s - c_r)\}$$

$$\tilde{h}_r^-(\bar{u}_s) \doteq h_r^-(\bar{u}_s) \cap \mathcal{D}_\gamma^r = \{m_r, c_r \in \mathcal{D}_\gamma^r : \bar{y}_s - \Delta\eta_s = m_r(\bar{u}_s - c_r)\}$$

Proposed solution: first-stage

Definition 4 (Constraints intersections)

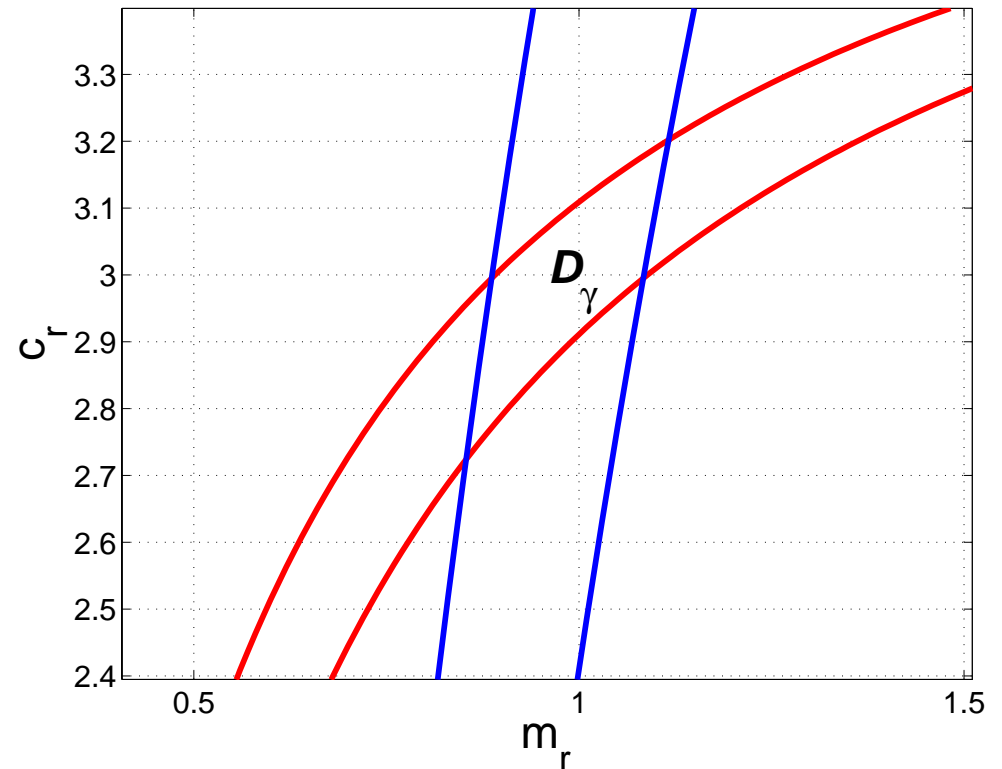
$$\mathcal{I}_\gamma^r = \{(m_r, c_r) \in \mathbb{R}^2 : \{h_r^+(\bar{u}_i), h_r^-(\bar{u}_i)\} \cap \{h_r^+(\bar{u}_j), h_r^-(\bar{u}_j)\} \neq \emptyset; i, j = 1, \dots, M; i \neq j\}$$

Definition 5 (Vertices of \mathcal{D}_γ^r)

$$\mathcal{V}(\mathcal{D}_\gamma^r) = \mathcal{I}_\gamma^r \cap \mathcal{D}_\gamma^r.$$

Remarks:

- An **exact description** of \mathcal{D}_γ^r can be given in terms of **edges** and **vertices**.
- A **recursive algorithm** for the **computation** of **edges** and **vertices** of \mathcal{D}_γ^r has been provided.



Proposed solution: first-stage

Tights bounds on $\gamma_1 = m_r$ and $\gamma_2 = c_r$ obtained computing the **orthotope outer-bound**:

$$\mathcal{B}_\gamma^r = \{\gamma \in \mathbb{R}^2 : \gamma_j = \gamma_j^c + \delta\gamma_j, |\delta\gamma_j| \leq \Delta\gamma_j, j = 1, 2\}$$

$$\gamma_j^c = \frac{\gamma_j^{\min} + \gamma_j^{\max}}{2}, \quad \Delta\gamma_j = \frac{|\gamma_j^{\max} - \gamma_j^{\min}|}{2}$$

$$\gamma_j^{\min} = \min_{\gamma \in \mathcal{D}_\gamma^r} \gamma_j, \quad \gamma_j^{\max} = \max_{\gamma \in \mathcal{D}_\gamma^r} \gamma_j. \quad (3)$$

- \mathcal{B}_γ is obtained solving problems (3) which are 2 **nonconvex optimization** problems with 2 variables and $2M$ constraints.
- **Main Result 1:**
The **global optimal** solutions of problems (3) **occur on the vertices** of \mathcal{D}_γ^r .

Proposed solution: second-stage

2) Bounds on the inner signal x_t

Result 1

The input of the backlash u_t is a PRBS with levels $\pm u^*$, $u^* > c_r$, $-u^* > c_l$



The output of the backlash x_t is a PRBS with levels $\bar{x}^* = m_r(u^* - c_r)$, $\underline{x}^* = m_l(u^* - c_l)$.

- **Bounds on the inner signal level x^*** are computed as:

$$\bar{x}^{*min} = \min_{m_r, c_r \in \mathcal{D}_\gamma^r} m_r(u^* - c_r), \quad \text{for } u^* \geq c_r \quad (4)$$

$$\bar{x}^{*max} = \max_{m_r, c_r \in \mathcal{D}_\gamma^r} m_r(u^* - c_r), \quad \text{for } u^* \geq c_r \quad (5)$$

Proposed solution: second-stage

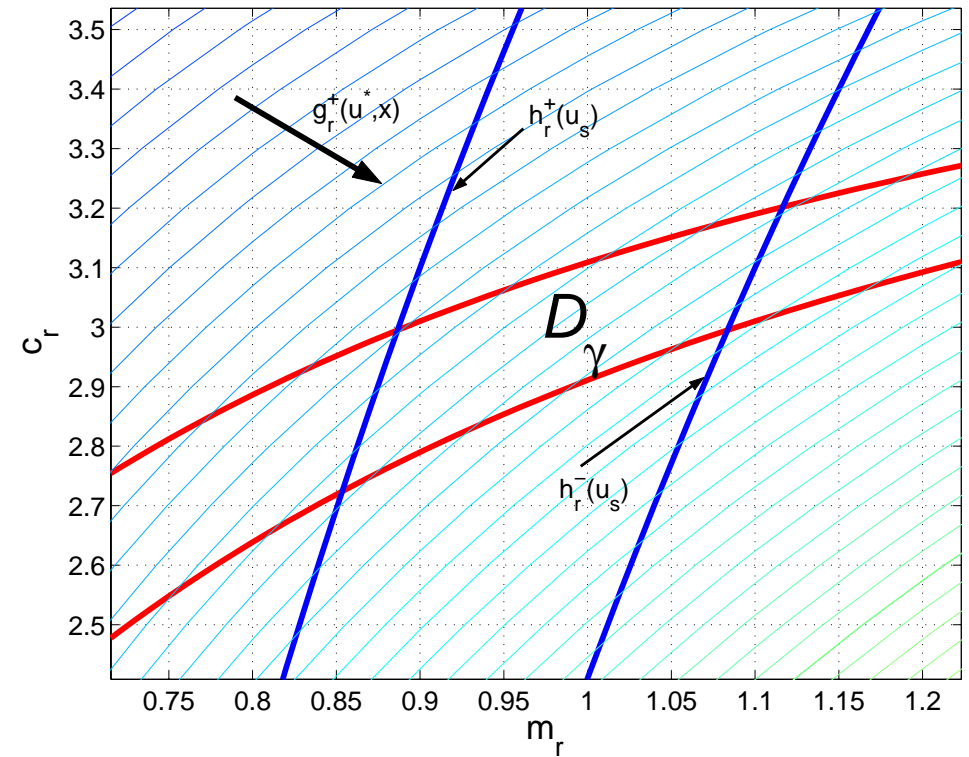
Definition 6 (x-level curve of the objective function to be optimized)

$$g_r(u^*, x) \doteq \{m_r \in \mathbb{R}^+, c_r \in \mathbb{R}^+ : x = m_r(u^* - c_r)\}$$

Main Result 2

(Computation of the inner signal bounds)

The **global optimal solutions** of problems (4) and (5) **occur on the vertices** of \mathcal{D}_γ^r .



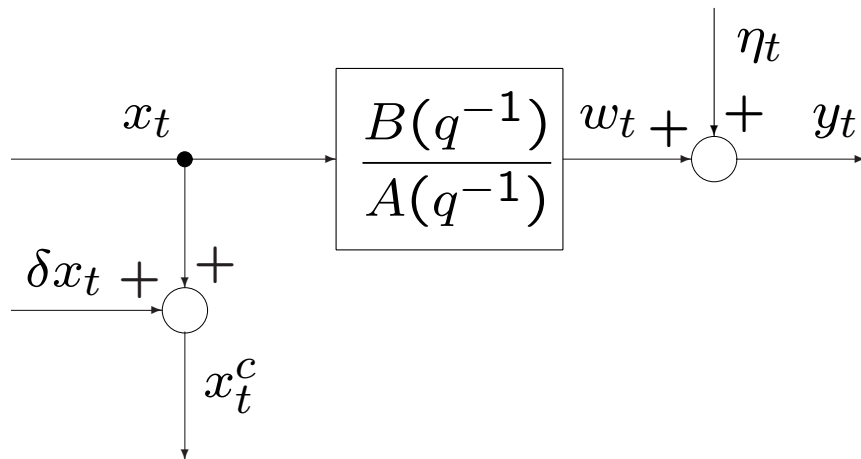
Proposed solution: third-stage

3) Bounds on the linear block parameters

The **input PRBS** sequence $\{u_t\}$ of levels $\pm u^*$ is applied and the (noisy) output sequence $\{y_t\}$ is measured.



Errors-in-variables (EIV) problem with UBB errors



$$x_t^c = \frac{\bar{x}^{*min} + \bar{x}^{*max}}{2}$$

$$|\delta x_t| \leq \Delta x_t$$

$$\Delta x_t = \frac{\bar{x}^{*max} - \bar{x}^{*min}}{2}$$

Proposed solution: EIV problem

Exploiting **previous results** on static EIV problem with bounded errors

(V. Cerone, "Feasible parameter set of linear models with bounded errors in all variables", *Automatica* 1993)



a polytopic outer approximation \mathcal{D}'_θ of the **feasible parameter set** \mathcal{D}_θ is characterized by:

$$(\phi_t - \Delta\phi_t)^\top \theta \leq y_t + \Delta\eta_t, \quad (\phi_t + \Delta\phi_t)^\top \theta \geq y_t - \Delta\eta_t$$

$$\phi_t^\top = [-y_{t-1} \dots -y_{t-na} \ x_t^c \ x_{t-1}^c \dots x_{t-nb}^c]$$

$$\Delta\phi_t^\top = [\Delta\eta_{t-1} \text{sgn}(a_1) \ \dots \ \Delta\eta_{t-na} \text{sgn}(a_{na})$$

$$\Delta x_t \text{sgn}(b_0) \ \Delta x_{t-1} \text{sgn}(b_1) \ \dots \ \Delta x_{t-nb} \text{sgn}(b_{nb})]$$

$$[1 \ \dots \ 1 \ -1 \ -1 \ \dots \ -1] \theta = -1$$

Proposed solution: EIV problem

Parameter uncertainty intervals $\Delta\theta_j$ are **provided by** the bounding orthotope \mathcal{B}_θ :

$$\mathcal{B}_\theta = \{\theta \in \mathbb{R}^p : \theta_j = \theta_j^c + \delta\theta_j, |\delta\theta_j| \leq \Delta\theta_j/2, j = 1, \dots, p\},$$

$$\theta_j^c = \frac{\theta_j^{min} + \theta_j^{max}}{2},$$

$$\Delta\theta_j = |\theta_j^{max} - \theta_j^{min}|,$$

$$\theta_j^{min} = \min_{\theta \in \mathcal{D}'_\theta} \theta_j, \quad \theta_j^{max} = \max_{\theta \in \mathcal{D}'_\theta} \theta_j.$$

Computational aspects:

- θ_j^{min} and θ_j^{max} are computed by means of linear programming techniques.

Example:

Parameters of the simulated system:

$$m_l = 0.24, m_r = 0.26, c_l = 0.035, c_r = 0.070;$$

$$A(q^{-1}) = (1 - 0.5q^{-1} - 0.1q^{-2});$$

$$B(q^{-1}) = (0.2q^{-1} + 1.2q^{-2})$$

Measurement output errors:

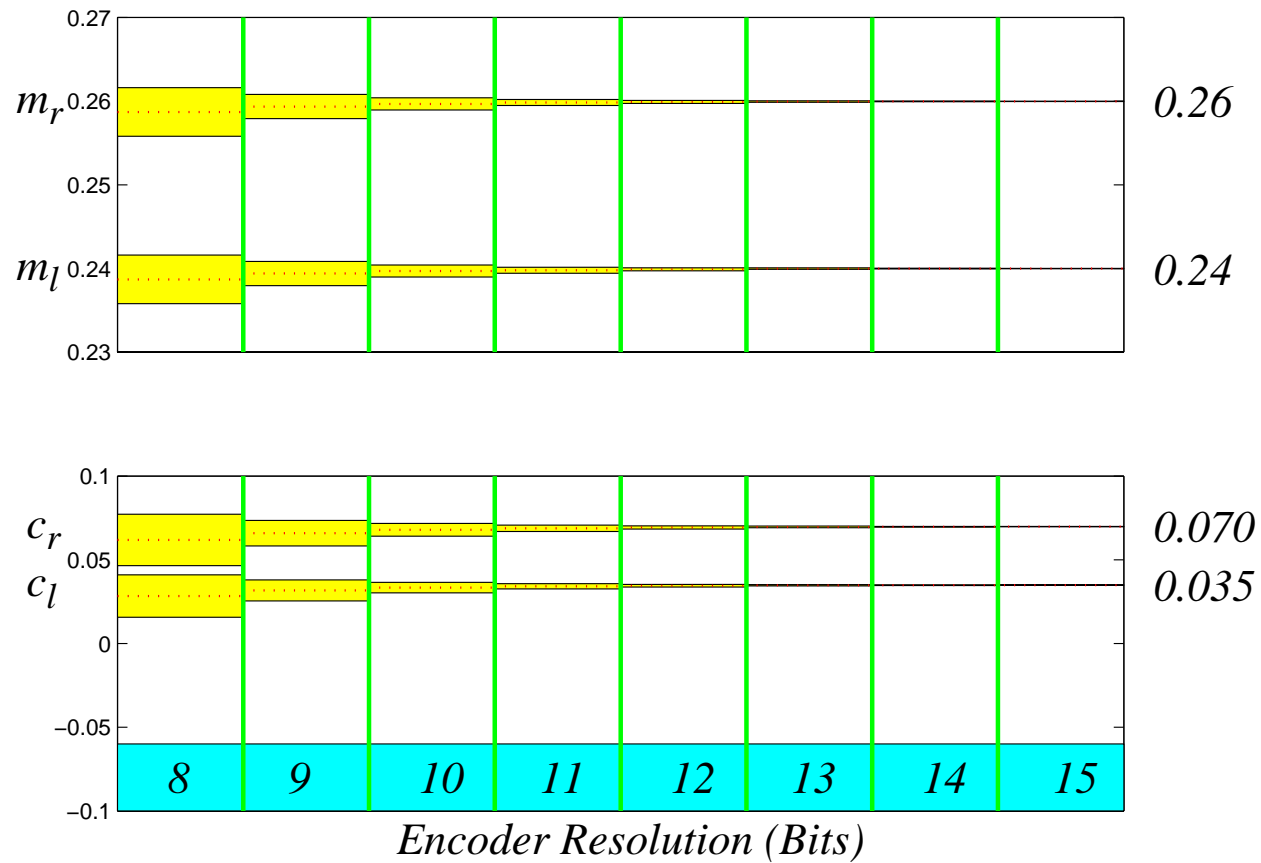
Bounded absolute output errors have been considered:

$$|\eta_t| \leq \Delta\eta_t; \quad \{\eta_t\} \text{ belongs to the uniform distribution } U[-\Delta\eta_t, +\Delta\eta_t].$$

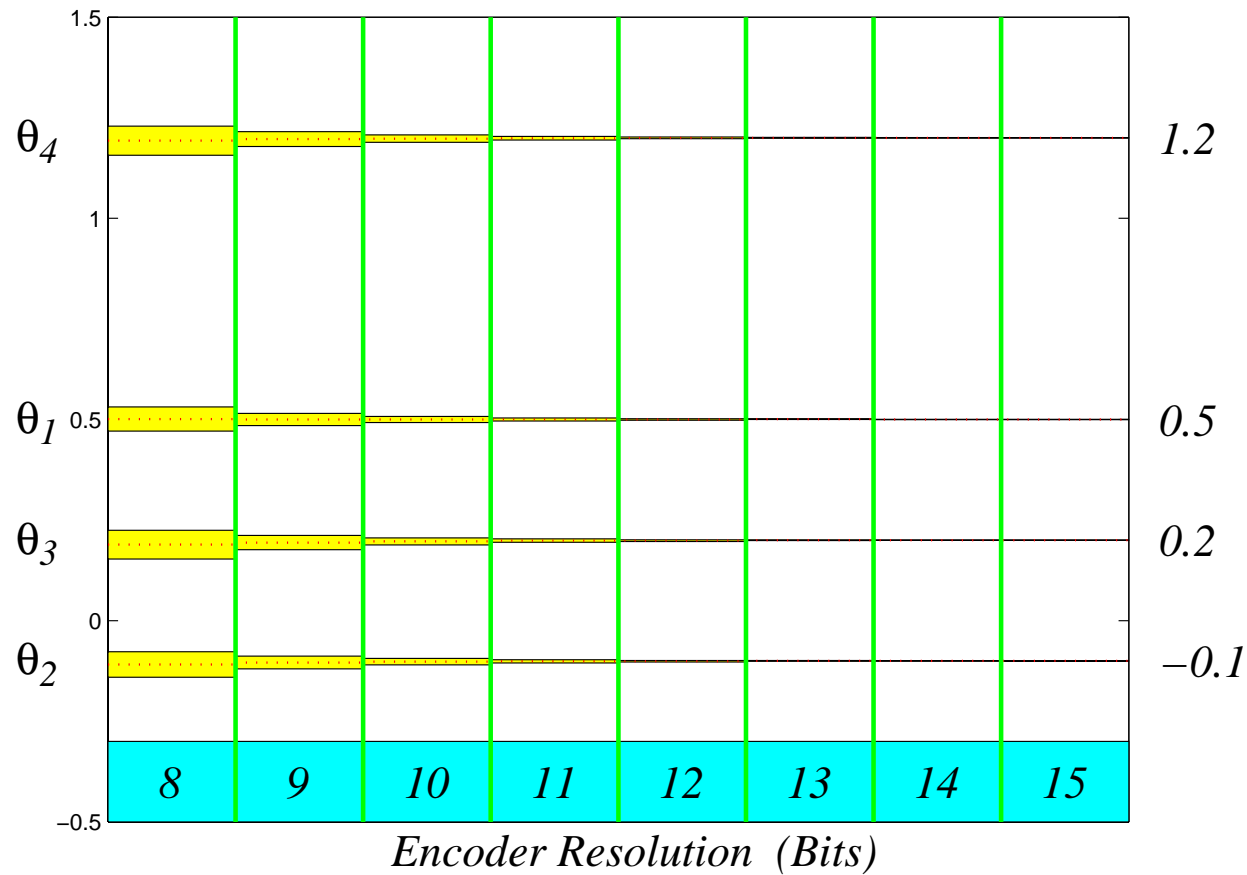
$$|\bar{\eta}_s| \leq \Delta\bar{\eta}_s; \quad \{\bar{\eta}_s\} \text{ belongs to the uniform distribution } U[-\Delta\bar{\eta}_s, +\Delta\bar{\eta}_s]$$

Eight different values of $\Delta\eta = \Delta\eta_t = \Delta\bar{\eta}_s$ were chosen in such a way to simulate the errors of eight commercial absolute binary encoder with number of bits n_{bits} varying from 8 to 15.

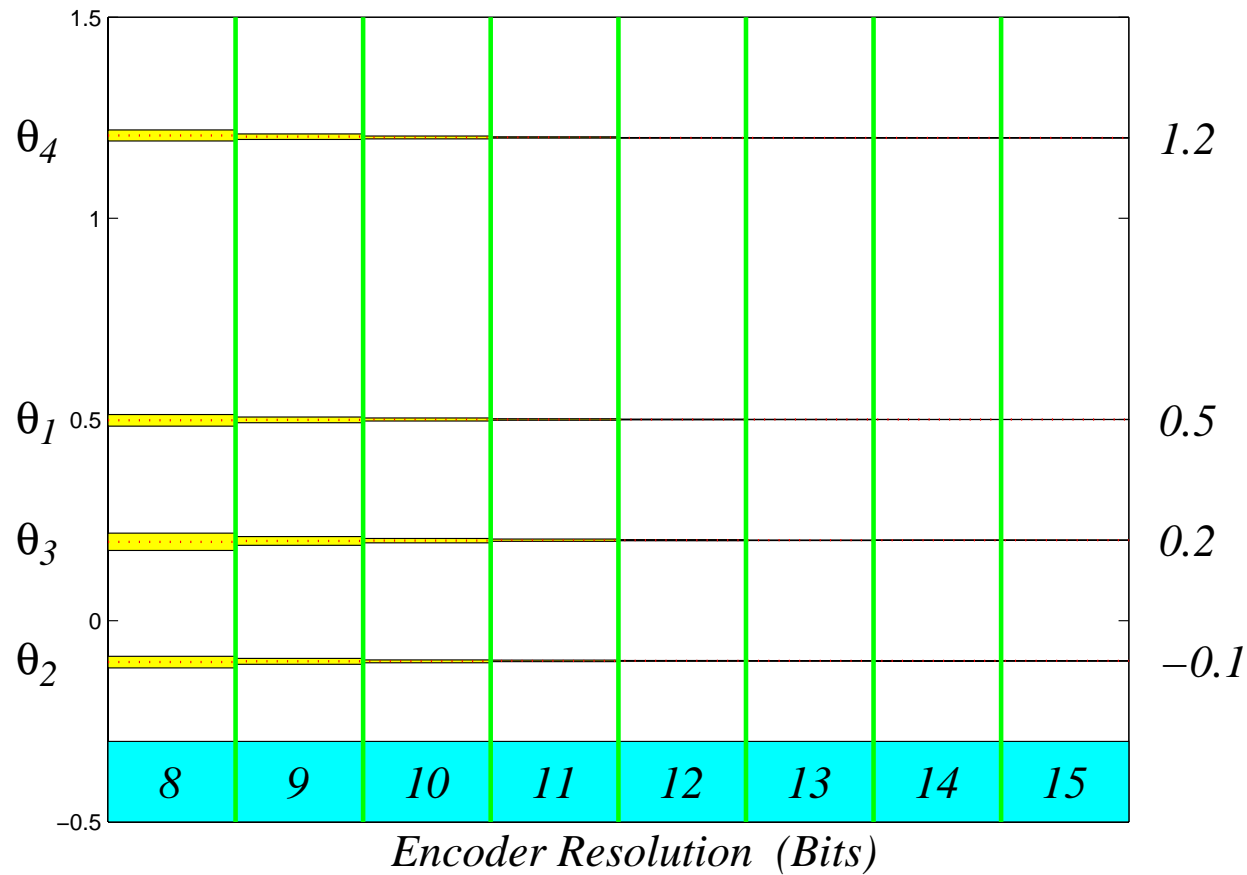
Backlash parameters: central estimates and parameters uncertainty bounds ($M = 50$)



Linear block parameters: central estimates and parameters uncertainty bounds (N = 100)



Linear block parameters: central estimates and parameters uncertainty bounds (N = 1000)



Conclusions

- The proposed three-stage parameter bounding procedure provides:
 - **tight bounds** on the parameters of the **backlash** using steady-state input-output data;
 - **overbounds** on the parameters of the **linear part**, through the computation of tight bounds on the unmeasurable inner signal x_t ;
- The numerical example has showed the effectiveness of the proposed procedure.
- The approach is computationally tractable: **the computation related to the above example (M=2, N=[100,1000]) required few seconds on a standard notebook (AMD 3200)**

[Reference paper](#)

References

Motivating papers

- M. Nordin, P. O. Gutman, “Controlling mechanical systems with backlash: A survey,” *Automatica*, vol. 38, pp. 1633–1649, 2002.
- M. Corradini, G. Orlando, and G. Parlangeli, “A VSC approach for the robust stabilization of nonlinear plants with uncertain nonsmooth actuator nonlinearities: A unified framework,” *IEEE Trans. Autom. Control*, vol. 49, no. 5, pp. 807–813, May 2004.
- G. Tao, C. Canudas deWit, Eds., “Special issue on adaptive systems with non-smooth nonlinearities,” *Int. J. Adapt. Control Signal Process.*, vol. 11, no. 1, 1997.

Identification

- E. Bai, “Identification of linear systems with hard input nonlinearities of known structure,” *Automatica*, vol. 38, pp. 853–860, 2002.
- V. Cerone, D. Regruto, “Bounding the Parameters of Linear Systems With Input Backlash,” *IEEE Trans. Autom. Control*, vol. 52, no. 3, pp. 531–536, March 2007.
- V. Cerone, “Feasible parameter set for linear models with bounded errors in all variable,” *Automatica*, vol. 29, no. 6, pp. 1551–1555, 1993.